

## EMC “Myths Versus Reality” #2

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### ***SYSTEM-PRODUCT RESPONSE TO ELECTROSTATIC DISCHARGE EVENTS***

The myth: A system-product that successfully complies with the criteria of ESD (IEC-based) Standards, will not exhibit personnel ESD susceptibility when used in actual installations.

The reality: The ESD “simulation” of typical “standards” only represents a portion of the ESD continuum that can be exhibited in nature.

Electrostatic Discharge (ESD) events from personnel in nature (as opposed to simulations stipulated in “standards”) exhibit a great variety of waveforms and peak amplitudes of current that are far broader in spectral impact than those required in “standards”. For example, at initialization ESD voltages (the static level prior to displacement through discharge) below approximately 5kV, research has shown that rise times can often be found in the 200 to 500 picosecond range with peak currents in the tens of Amperes. As initialization voltages increase, the ionization path at the discharge point increases and the rise times can slow down into the range of approximately 1 to 20 nanoseconds. Peak currents, however, at these slower rise times can still be found in the range of tens of amperes for conditions where the ESD comes from a metal object (e.g. a key). [Currents from fingertips in nature are much less, by an approximate factor of 5.]

Extending the continuum of ESD events into further conditions, such as ESD from mobile-furnishings (e.g. desk chair structures that can impact “horizontal” planes) brings even increased peak currents (approaching 100 Amperes from source impedance of approximately 75 Ohms) and increased radiated field intensities (from the displacement of current in the structure). The extraordinary current peaks from “mobile furnishings” pose an increased threat to system performance simply due to the current stress. The high current from ESD at, for example, 15 kV from a metal push-cart can produce time-domain radiated field intensities from the cart (which will become a transmitting antenna with the ESD current displacement) in the range of approximately 1,600 Volts/meter!

In practice, ESD impulses are spectral excitations across a broad frequency span. The “efficiency” of spectral excitation is established by the rise time, while the intensity is established by the current delivered to the system-product. At low (ESD) voltages where the rise times tend to exhibit a spectral distribution well over 1 GHz, system-products may be more responsive (susceptible) due to the “match” of the ESD spectra to fast circuit devices than at higher ESD voltages where the rise times are much slower. Spectra from longer ESD rise times can influence responses in interface cables (which can support the lower-spectra of current) where the spectra from faster rise times can couple through local “apertures” in shields or circuit devices to cause system response.

Considered in combination, it is possible for a system to exhibit ESD responses to lower ESD voltages ) e.g. 2 to 4kV), and not higher voltages, OR, mid-ESD range voltages (e.g 5 to 8 kV) and not lower or higher levels (sometimes called “the response window effect”), OR, simply, only “higher” (>10kV) levels. This assumes, however, that in performing such evaluations on products the ESD Test Generator used is capable of producing the ESD waveforms that are variable at different voltages as they are found in nature. The effect noted here can be termed the “spectral-bandwidth-dependency” for response, where the spectral bandwidth is defined by the ESD amplitude in nature. The description also exposes another “myth”: That testing a system-product at high ESD amplitudes will assure immunity at lower amplitudes.

Given these realities combined with the limitations of “standard” test methods, the typical immunity tests may be viewed as only “tentative” in describing the ESD performance of system-products.